



# Transverse Rupture Strength of CeO<sub>2</sub> as a Surrogate Nuclear Fuel

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## Background

### Nuclear Energy

- Currently, 20% of the US energy demand is supported by nuclear energy and is increasing, creating a growing interest in fully understanding the relationship between microstructure and performance of ceramic nuclear fuels<sup>1</sup>.
- Plutonia (PuO<sub>2</sub>), recovered as a by-product from the fission of uranium, is of particular interest.
- Because of significant challenges involved in studying radioactive materials, cerium oxide (CeO<sub>2</sub>) is being investigated as a surrogate nuclear fuel for PuO<sub>2</sub> due to having similar chemical and thermodynamic properties<sup>2</sup>.

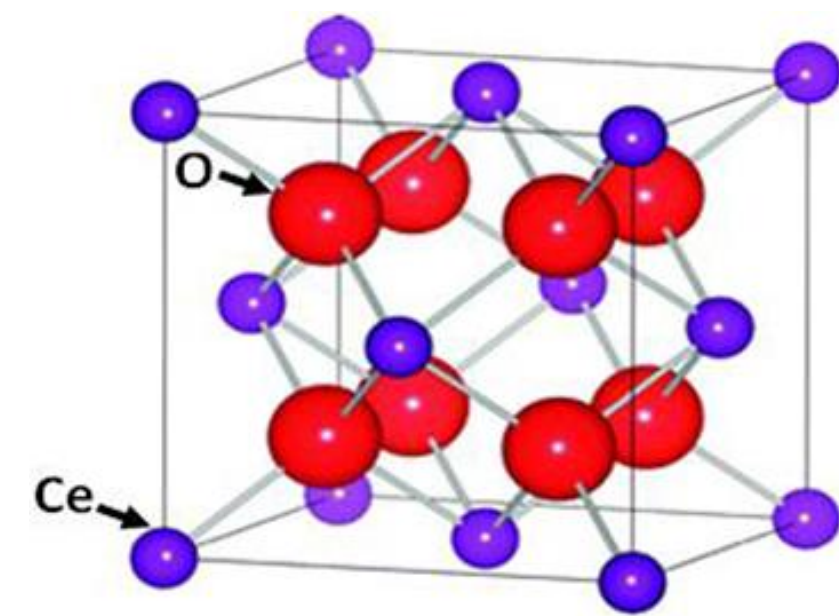


Figure 1. Cerium oxide has the same crystal structure as plutonium oxide, which is an Fm3m fluorite structure<sup>3</sup>.

### Surrogate Nuclear Fuel Study of CeO<sub>2</sub>

- Mechanical properties of CeO<sub>2</sub> were studied through developing and validating a testing method for testing its flexural strength.
- Test method was validated using commercially available alumina (Al<sub>2</sub>O<sub>3</sub>), with known properties, as a benchmark.
- CeO<sub>2</sub> pellets were fabricated and characterized prior to measuring flexural strength.

## Methods

### CeO<sub>2</sub> Pellet Synthesis

- Materion (-325 mesh) CeO<sub>2</sub> powder was high energy ball milled to reduce particle size and improve pellet density.
- CeO<sub>2</sub> powder and EBS binder were mixed and green pellets were pressed at 100 MPa and sintered at 1600 °C.
- CeO<sub>2</sub> powder and pellets were characterized via scanning electron microscopy (SEM), x-ray diffraction (XRD) and particle size analysis (PSA).
- Sintered pellets were ground down to 169 μ" and 11 μ" surface roughness.
- CeO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> were tested using the test fixture and Materials Test System 810 in Figure 7.

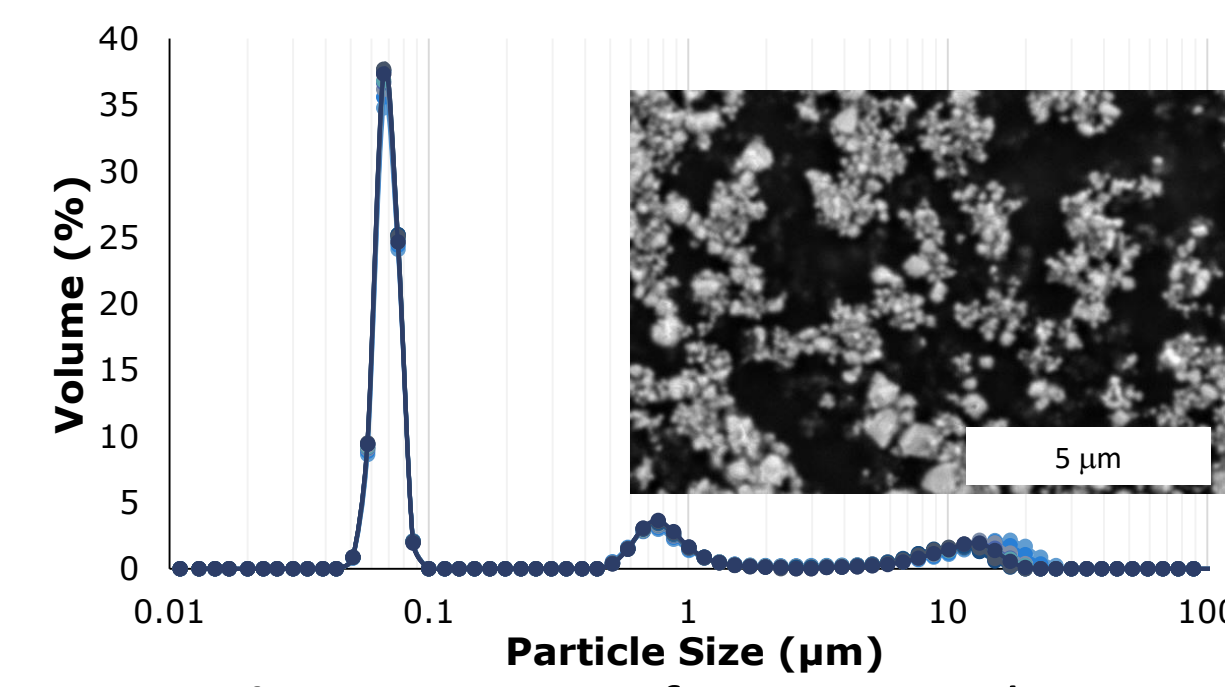


Figure 2. SEM of CeO<sub>2</sub> powder and particle size distribution.



Figure 3. Sintered ceria pellet pressed at 100 MPa.

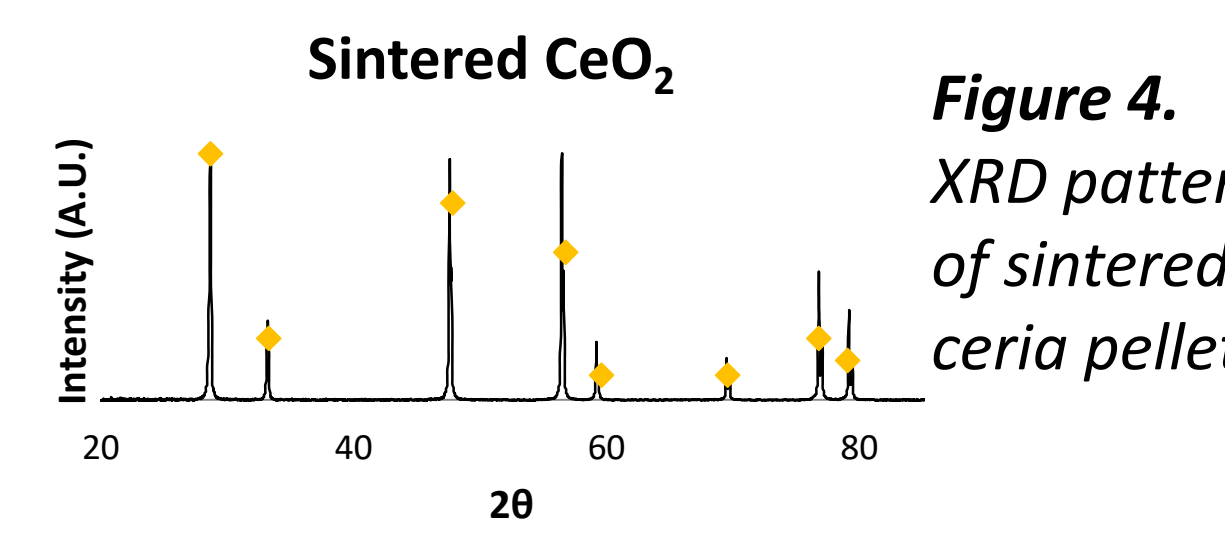


Figure 4. XRD pattern of sintered ceria pellet.

### Al<sub>2</sub>O<sub>3</sub> Benchmark Preparation

- 99.8% purity Al<sub>2</sub>O<sub>3</sub> rods (Figure 5) were cut at 1.5, 2.25, and 3 mm heights and ground down to 169 μ" and 11 μ" surface roughness.

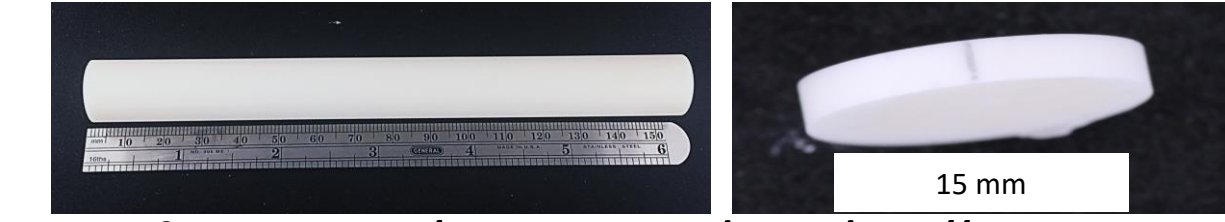


Figure 5. Alumina rod and pellet.

## Results

### Transverse Rupture Strength Setup

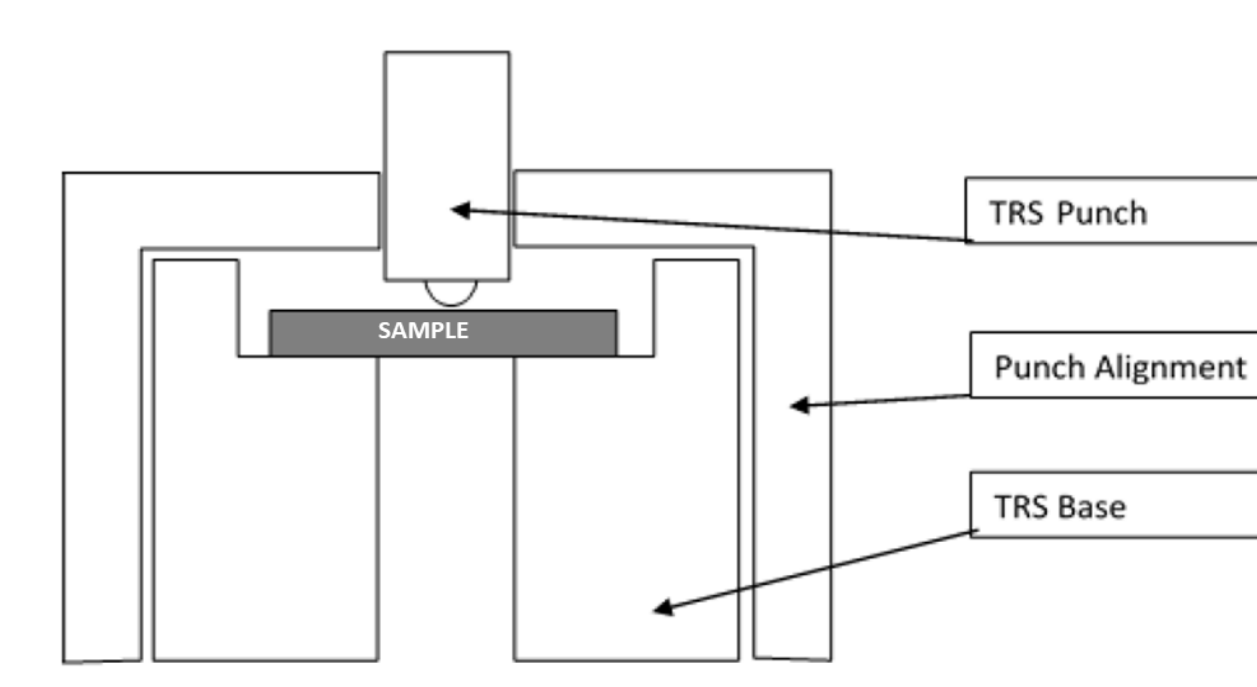


Figure 6. Schematic representation of transverse rupture strength fixture.



Figure 7. MTS-TRS setup.

### Transverse Rupture Strength Equation

$$\sigma = \frac{A * F}{t^2}$$

A = effective stress volume  
F = force applied to pellet at failure  
t = pellet radius  
σ = transverse rupture strength<sup>6</sup>

### Al<sub>2</sub>O<sub>3</sub> Transverse Rupture Strength

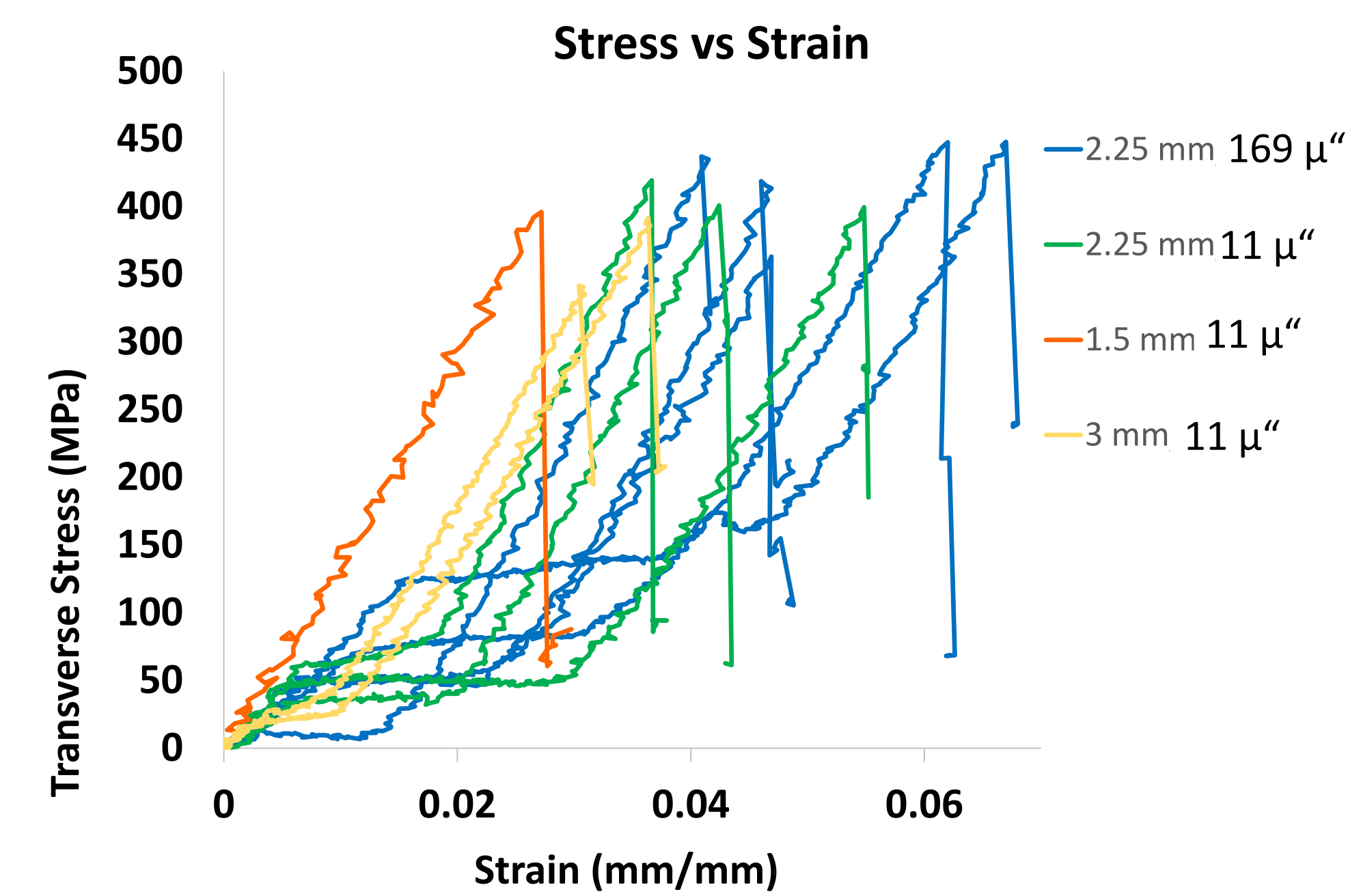


Figure 8. Transverse stress vs Strain plot of Al<sub>2</sub>O<sub>3</sub>.

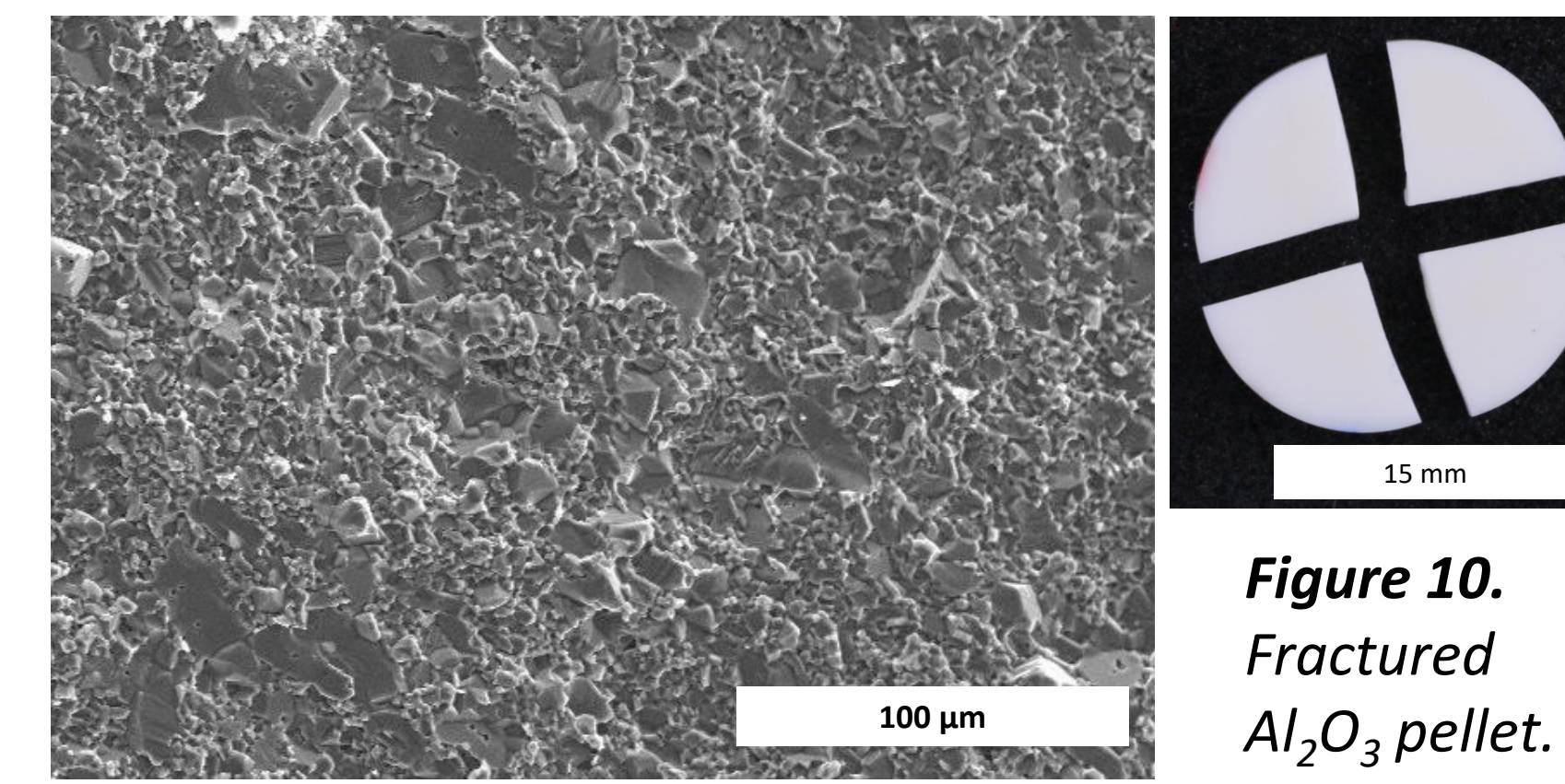


Figure 9. SEM image of alumina fracture surface.

Number of Tests	Density	Surface Roughness	TD %	Flexural Strength (MPa)
6	3.87 g/cm <sup>3</sup>	169 μ"	98.8 ± 0.2	363-448
6	3.87 g/cm <sup>3</sup>	11 μ"	98.8 ± 0.2	341-419

Figure 11. Alumina pellet data table. Theoretical density based on 3.92 g/cm<sup>3</sup> as provided by the vendor<sup>5</sup>.

### CeO<sub>2</sub> Transverse Rupture Strength

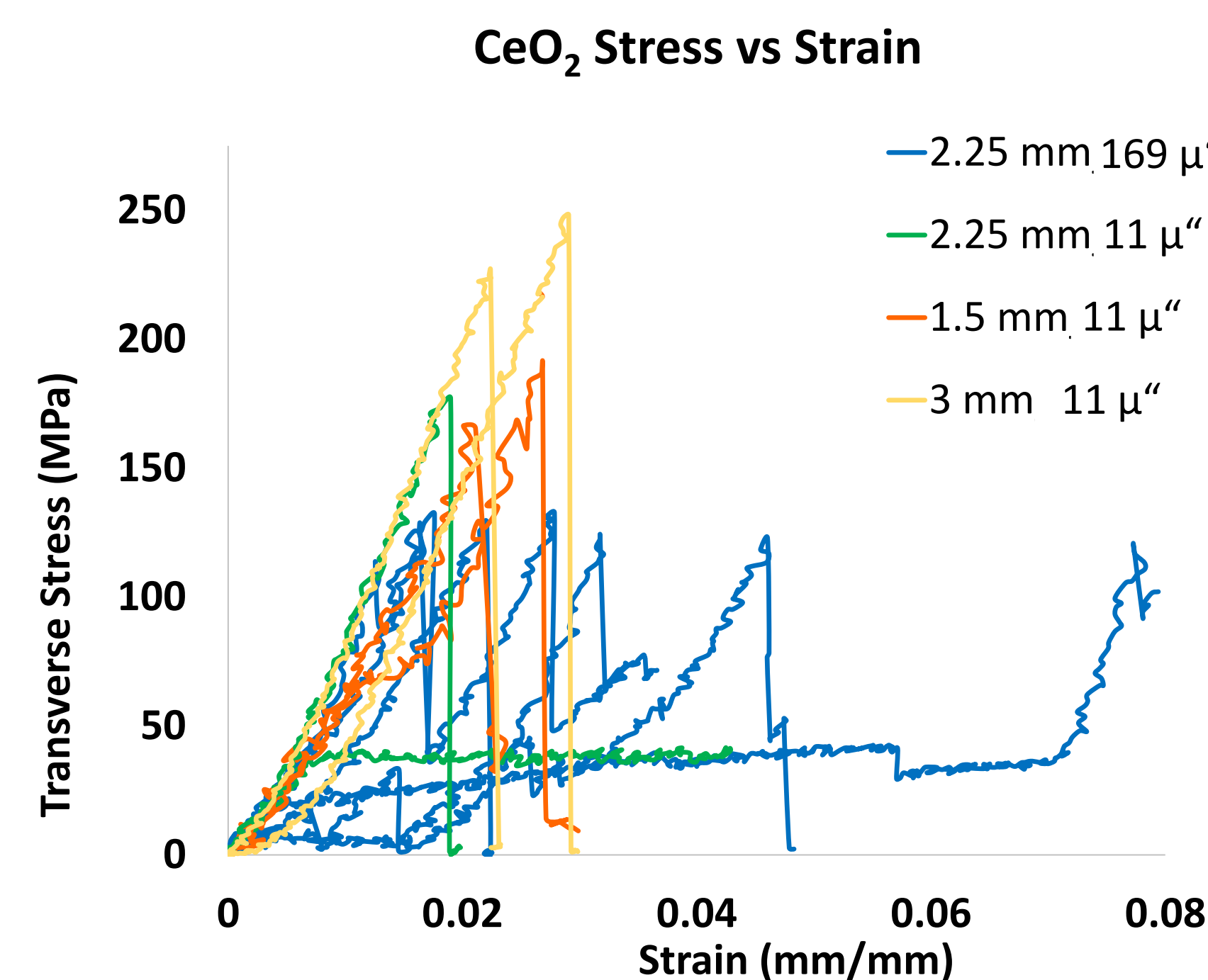


Figure 12. Transverse stress vs Strain plot of CeO<sub>2</sub>.

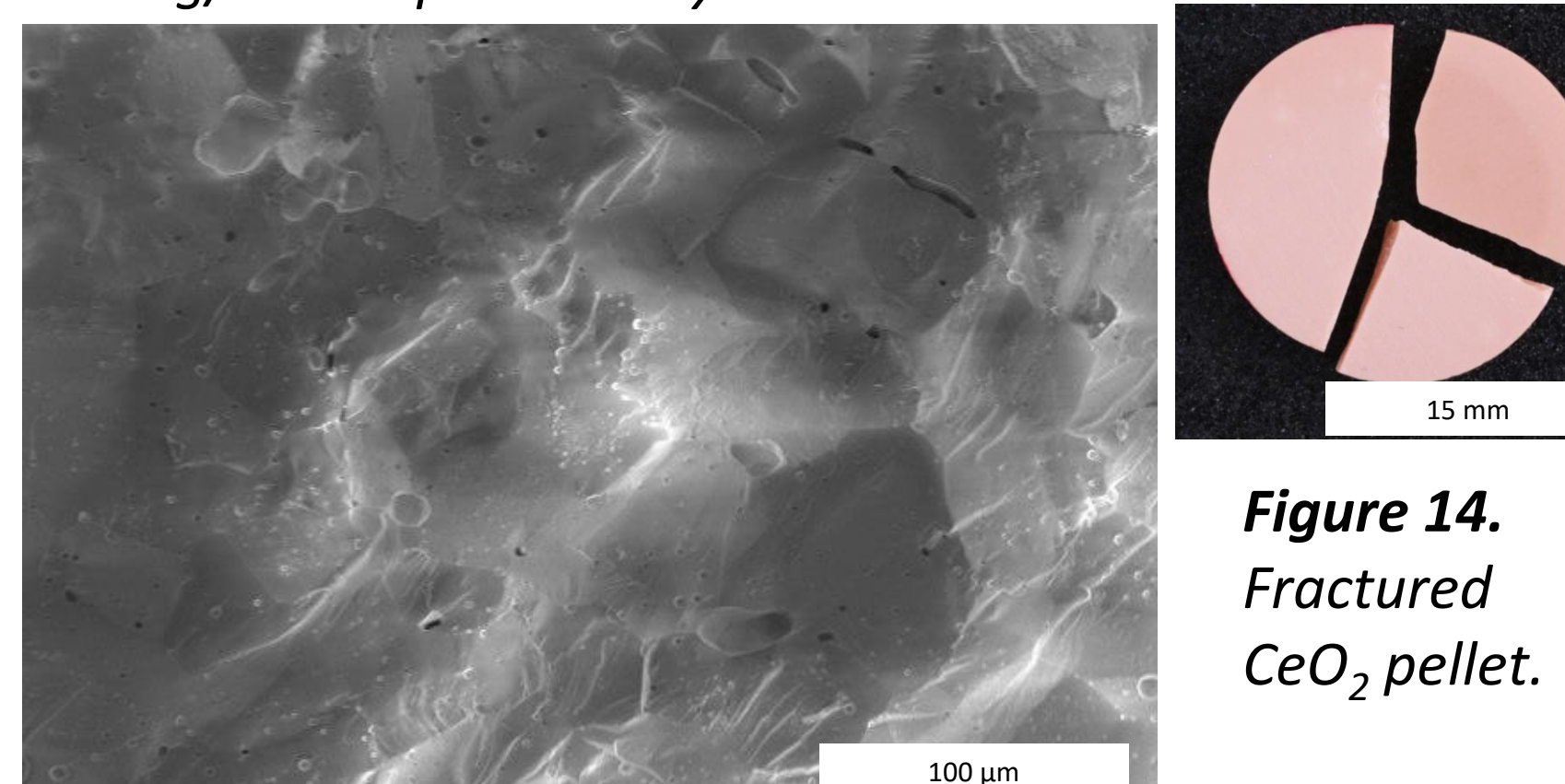


Figure 13. SEM image of ceria fracture surface.

Number of Tests	Sintered Density	Grain Size	Surface Roughness	TD %	Flexural Strength (MPa)
6	6.83 g/cm <sup>3</sup>	28 μm ± 2	169 μ"	95.8 ± 2	40.5-132
6	6.83 g/cm <sup>3</sup>	28 μm ± 2	11 μ"	95.8 ± 2	41.7-248

Figure 15. Ceria pellet data table. Theoretical density based on literature value of 7.21 g/cm<sup>3</sup>,<sup>6</sup>.

## Discussion

### Transverse Rupture Strength

$$A = \frac{3}{4 * \pi} * \left[ \left( 2 * (1 + \nu_s) * \ln \frac{a}{b} \right) + \frac{(1 - \nu_s)(2a^2 - b^2)}{2 * R^2} + (1 + \nu_s) \right]$$

#### Test Sample

ν<sub>S</sub>: 0.21 alumina    b =  $\sqrt[3]{\frac{6 * F * (1 - \nu_B) * r}{E}}$

#### Test Fixture

ν<sub>B</sub>: 0.21 (tungsten carbide<sup>7</sup>)  
E: 600 GPa (tungsten carbide)

ν<sub>S</sub>: Poisson's ratio of material  
a: radius of support circle  
R: radius of sample (7.95 mm)  
b: contact radius of loading ball  
ν<sub>B</sub>: Poisson's ratio of loading ball  
r: radius of loading ball  
E: Elastic Modulus of loading ball

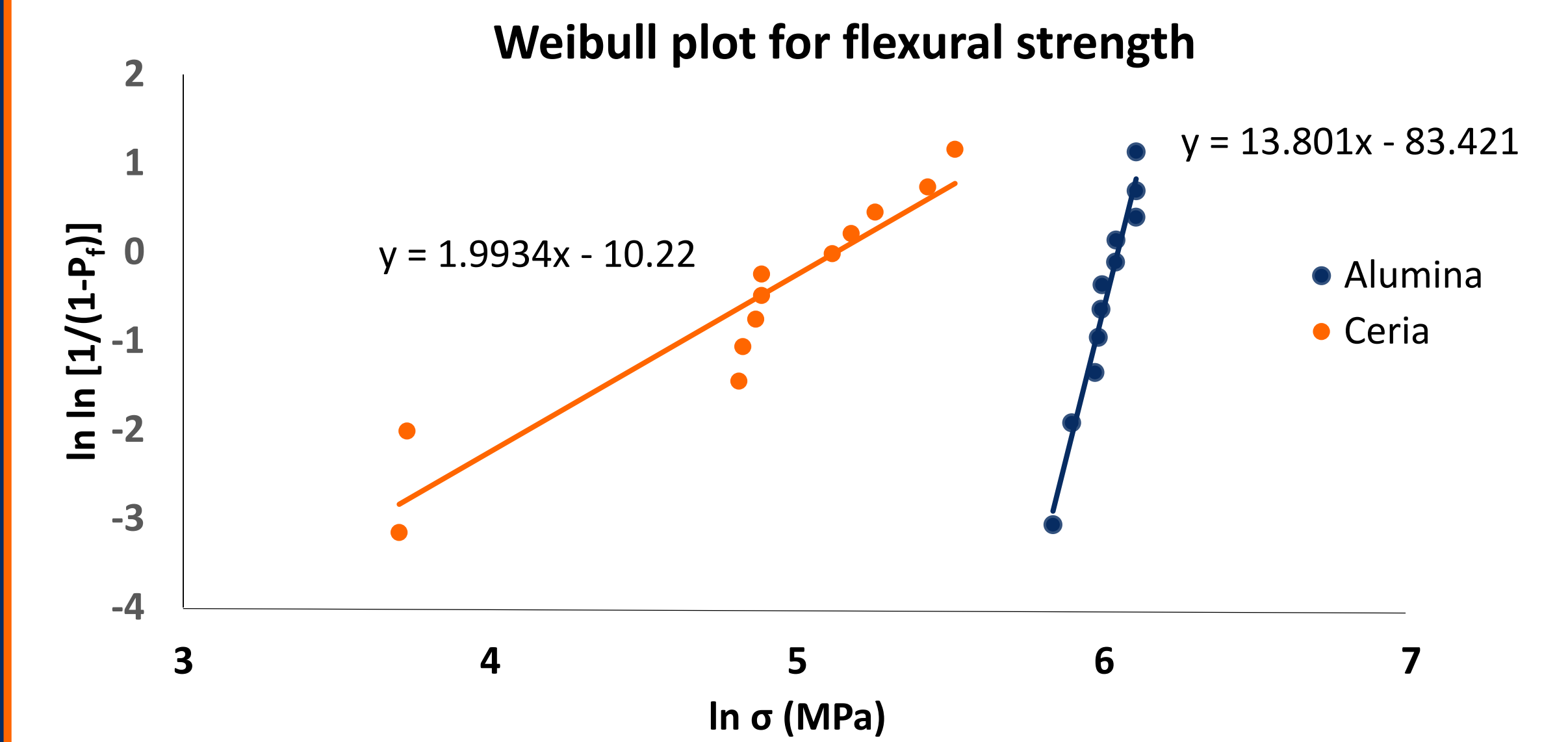


Figure 16. Weibull plots of the flexural strength data of alumina and ceria.

### Effects of Microstructure

- Grain size, density, porosity, bulk/surface defects, and surface roughness affect flexural strength and Weibull modulus.
- Ceria pellets had an average grain size (Figure 17) of ~28 μm.
- Pellets had an average of 95.8% ± 2 theoretical density.
- The high Weibull modulus for alumina demonstrates the validity of the MTS-TRS set up.

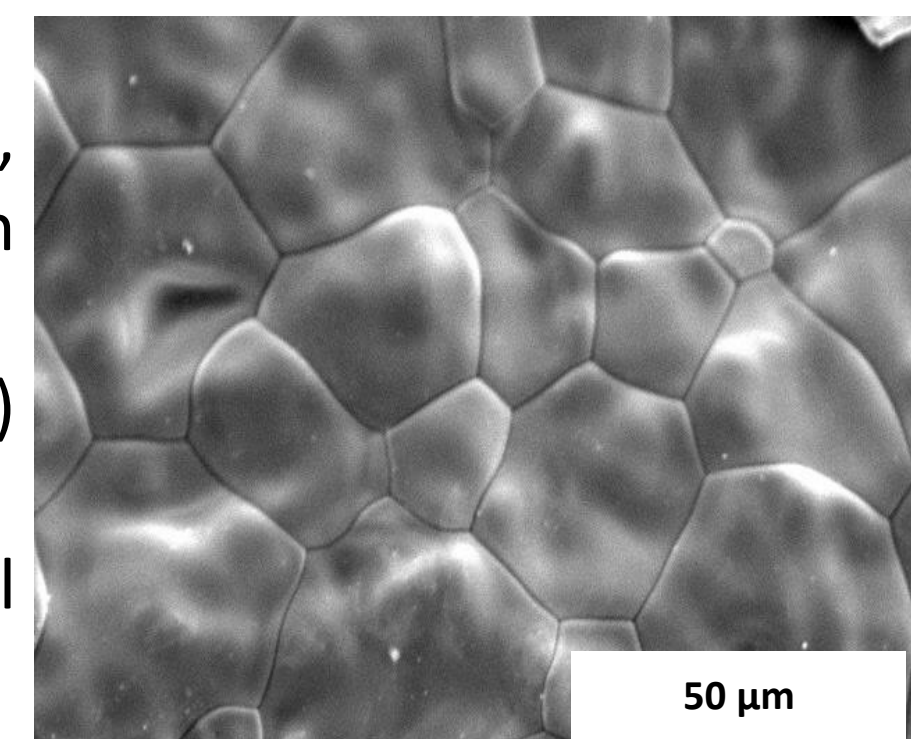


Figure 17. SEM of CeO<sub>2</sub> grains.

### Challenges

- Alumina grain size for comparison to literature and ceria.
- Further validation tests for the TRS set up using magnesia partially-stabilized zirconia and yttria stabilized zirconia as benchmarks.
- Thermogravimetric analysis to address delamination and stoichiometry issues in ceria.

### Conclusions

- Alumina flexural strength is comparable to literature values<sup>5</sup>, 375 ± 54 MPa.
- Weibull modulus for alumina supports the MTS-TRS setup.
- Flexural strength for ceria was improved with a finer surface finish and greater height to diameter ratio.
- Weibull modulus for ceria can be improved by microstructure refinement.

## References

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